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POINT OF VIEW

Clinical implications of the rheological theory in the prevention of ventilator-induced lung injury. Is mechanical power the solution?☆

Implicaciones clínicas de la teoría reológica en la prevención de la lesión pulmonar inducida por el ventilador. ¿Es la potencia mecánica la solución?

V. Modesto i Alapont^a, M. Aguar Carrascosa^b, A. Medina Villanueva^{c,*}

^a Unidad de Cuidados Intensivos Pediátricos, Hospital Universitari i Politècnic La Fe, València, Spain

^b Unidad de Cuidados Intensivos Neonatales, Hospital Universitari i Politècnic La Fe, València, Spain

^c Unidad de Cuidados Intensivos Pediátricos, Hospital Universitario Central de Asturias, Oviedo, Spain

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Rheology describes the relation between stress (tension) supported by a material and the strain (deformation) induced in this material by an applied force. The concepts related with the Rheology, based on experimental results in animals and in humans, seems to be the most plausible explanation for Ventilator Induced Lung Injury (VILI).

The objective of this paper is to analyse the clinical implications of the rheological theory and the relation between mechanical power and the development of VILI.

VILI is a time dependent phenomenon

Dynamic development VILI

In 2013 Gattinoni repeated their experiment of 2011 but this time with a prospective cohort design.¹ Healthy pigs were ventilated (inspired fraction of oxygen [FiO₂] = 0.5, respiratory rate [RR]: 15 breaths per minute [bpm]) with an end-inspiratory volume equal to the total lung capacity (TLC). Using different combinations of V_T and PEEP, they created four cohorts of pigs, each ventilated for 60 h with a different strain value: 2.5, 1.154, 0.556 and 0.217. The higher strain group had a higher histological damage of VILI and higher levels of local and systemic inflammatory markers.

However, the prospective design made it possible to temporally monitor the other cohort groups. They discovered a statistical relationship between *strain* and duration of ventilatory support:

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* Corresponding author.

E-mail address: amedinavillanueva@gmail.com

(A. Medina Villanueva).

- In the cohort where strain used was 2.5, VILI was detected at 6 h of ventilation and all subjects were dead by 48 h.
- In the cohorts where strain used was 1.154 and 0.556, VILI was detected at 24 and 36 h respectively. All subjects survived.
- Surprisingly the cohort where the strain used was 0.217, despite the fact they were ventilated for 60 h using end-inspiratory volumes equal to TLC (initial P_{plat} : $36 \pm 3 \text{ cmH}_2\text{O}$), not only was VILI not detected but also P_{plat} at the end of the experiment was the lowest of all the four cohorts.

Therefore, it is possible to conclude that VILI is a time-dependent phenomenon. It is important to highlight that none of the theories proposed to explain the pathogenesis of VILI (barotrauma, volutrauma, atelectrauma, biotrauma) have considered the importance of duration of ventilation.

Gattinoni and his research group experimentally studied the dynamics of the development of VILI related to time.² Thus, in healthy animals ventilated without PEEP and subjected to a strain of 2.5, they observed that the development of VILI occurred exponentially. Measuring with CT, they discovered that the presence of new densities in the pulmonary parenchyma:

- Started within 6 h of ventilation.
- In the interface areas of naturally non-homogeneous structures (especially in subpleural microatelectasis of the base, but also peribronchial and intraparenchymal areas).
- With time these expanded exponentially, bilaterally throughout the parenchyma.

These non-homogeneous zones in which VILI starts (*stress raisers*) act as a kind of “nuclei of crystallisation” in the exponential development of VILI. The development of VILI through a mechanism that implies the existence of stress raisers was deduced mathematically as early as 1970 by Mead.³ The concept of stress raisers is taken from material science. It is exactly the same mechanism which explains the so-called “*fatigue of materials*”. The internal nucleation and propagation of fractures that originate in microscopic areas around stress raisers, such as impurity particles, causing the material to be unstable and liable to failure under conditions of fluctuating stress.

An important discovery with practical implications was that these initial VILI densities (stress multipliers) appear only in the computer tomography slices performed during expiration. This means that stress raisers are highly recruitable areas, so by using high PEEP, their appearance is prevented and a more homogenous parenchyma is maintained. This would be therefore, a way to prevent the appearance of the precursory lesions of VILI.

Increasing the respiratory rate (RR) increases VILI

In 2000, Marini et al.⁴ described for the first time that a high RR worsened VILI in an animal model (rabbit lungs

isolated from the thorax and perfused “ex vivo”). However, the strongest evidence of the involvement of temporal factors (RR) has been provided by the team of researchers at the Karolinska Institute.⁵

In an experiment called “two-hit injury model” (VILI is generated by alveolar lavage with physiological serum followed by very aggressive ventilation for 2 h) they looked at two groups of animals; one with a RR of 20 bpm and the other with a RR of 40 bpm. All of them were ventilated with an ARDSnet strategy ($V_T = 6 \text{ mL/kg}$, $\text{PEEP} = 10 \text{ cmH}_2\text{O}$, $\text{FiO}_2 = 0.5$). They found that high RR group had worsened P/F ratio, biochemical and anatomopathological markers of VILI. This means that low RR protects the lungs from VILI in ARDS.

Clearly, these findings raise an interesting clinical question. Is “high-frequency” ventilation really protective?

High flow increases VILI production

The Gattinoni group performed an experiment using healthy pigs ventilated with volume controlled mode with a RR of 15 bpm and strain of 2.1 ± 0.9 .⁶ They were randomly divided into two groups: in one with low flows ($469 \pm 156 \text{ mL/s}$), $I:E$ ratios of 1:3 to 1:5 and a low strain rate. In the other, the high strain rate, high flows ($1322 \pm 246 \text{ mL/s}$) and $I:E$ ratios of 1:5 to 1:9. At the end of the experiment:

- The high strain rate group had worse compliance and P/F ratio.
- The high strain rate group had more inflammatory markers and anatomopathological signs of pulmonary oedema.
- The prevalence of VILI was 73% in the high strain rate group and 20% ($p=0.01$) in the other.
- At 54 h of ventilation 47% of the pigs in the high strain rate group had died and only 13% in the other group.

That is, in the production of VILI, not only the strain induced by the mechanical ventilator is important but also the speed in which the ventilator produces this strain rate. In conclusion, high velocities of flow induce deformation and therefore give rise to higher incidence of VILI.

In addition, an important clinical finding in these animals was that:

1. The higher VILI group had a higher value in the dynamic pulmonary hysteresis index (J)
2. They had a higher stress relaxation index (P1–P2 index; cmH_2O).

These two values can be calculated from the ventilator data.

Protti et al. detected that strain and strain rate interact with each other and increase both the dynamic hysteresis and P1–P2 index.⁶ This means that the lungs (as we have seen, viscoelastic bodies) behave more as viscous liquids than as elastic solids. And therefore, this particular behaviour increases VILI. Clinical staff therefore may be

able to program the ventilator with more optimal settings in order to prevent VILI if they monitor these two values.

From a practical point of view, it is important to highlight the influence of flow used in different ventilator modes. In a series of experiments designed to try to compare pressure controlled modes with adaptive targeting scheme (PC-CMVa; pressure controlled modes with target volume) and volume controlled modes (VC-CMV), in healthy animals and in animals with ARDS,⁷⁻⁹ the authors found a clear superiority of the VC-CMV modes, not only in the parameters of oxygenation but also in the anatomopathological measurements at autopsy. The PC-CMVa mode produced much more VILI and the authors proposed that the highest flow peak was responsible. It is possible that greater peak flow induces a higher strain rate and, as the Gattinoni team has demonstrated, this explains why more VILI can be produced.

What effect does PEEP have?

Currently, the effect of PEEP on the incidence of VILI has not yet been established experimentally from the rheology perspective based on the effect of stress and strain.

Theoretically, since increasing PEEP increases FRC and it is a key element of strain and strain rate, increasing lung recruitment by increasing PEEP should decrease VILI, although there exists contradictory results.

Data from two studies point in this direction.^{10,11} However, it is difficult to predict the effect of PEEP on pulmonary recruitment¹² at the bedside, as PEEP does not always increase FRC in patients with ARDS. This theory could be based on an erroneous and therefore a biased hypothesis.

The results of the clinical trials offer interesting results. Kassis et al.¹³ reexamined the data from their NEJM article in which an improvement in elastance and decrease in stress (ΔP_{TP}) had been demonstrated in patients with ARDS who were ventilated with an oesophageal pressure-directed strategy. This improvement was seen in those patients whom received higher PEEP during the first day. A case-control re-analysis found that the survivors (at 28 days) had been ventilated during the first day with a driving pressure (DP) less than 13 cmH₂O, a statistically lower value than the DP received by the patients who died (around 15 cmH₂O).

The Swedish Karolinska team has provided the most robust scientific evidence of the beneficial effect of PEEP on the development of VILI to date. They repeated their "two-hit injury model" study⁵ but with a significant modification: they applied a recruitment manoeuvre to identify the optimal PEEP. This was defined as 2 cmH₂O above the PEEP which maximised the dynamic compliance in a decremental manoeuvre.¹⁴ The animals in the experiment were ventilated with an *Open Lung Approach* (OLA) strategy however, the rest of the parameters were maintained as in their previous experiment (volume-control mode, $V_T = 6 \text{ mL/kg}$, $\text{FIO}_2 = 0.5$). The two study groups received respectively a RR of 20 bpm and 40 bpm. After

4–6 h of ventilation, the biochemical and anatomopathological VILI markers were indistinguishable between the two cohorts (high and low RR). These results were similar to those found in the lower RR cohort of the previous experiment (ARDSnet). Therefore, it can be concluded that in ARDS, PEEP prevents VILI caused by high RR.

Protti et al.⁶ came to similar conclusions. Both the low strain rate and high strain rate cohorts showed lower relaxation stress (P1–P2 difference) when ventilated with PEEP = 10 cmH₂O than with PEEP = 0 cmH₂O (ZEEP). There seems to be no relationship ($p = 0.994$) between the effect of PEEP and strain rate therefore PEEP appears to be an independent factor that decreases the viscous behaviour of the lung parenchyma when ventilated. It is not possible to determine causality based on those results but, as higher PEEP allows the ventilation of lungs with lower stress relaxation, it is possible to infer that it reduces VILI.

Integrating all concepts: mechanical power

The definitive step in the development of a complete theory that draws from rheology and materials engineering in order to scientifically explain the production of VILI has been the introduction of the concept of mechanical power (MP) by the team of Gattinoni in 2016. It allows the integration of all the different ventilator parameters that have been described as co-factors capable of producing VILI (V_T , pressures, frequency and flow) in a single physical quantity. The objective is to measure the mechanical energy that is transmitted to the respiratory system of the patient (airway + lung parenchyma) by the ventilator. All this energy expressed per time unit (J/min) is the MP.

For physicists, energy and work are interchangeable concepts. Energy is a measurement of "ability to perform a job", and work is "energy transferred by a force".

In classical physiology, respiratory work of breathing (WOB) during inspiration using constant flow ventilation¹⁵ is measured as:

$$\text{WOB} = \int P(t) dV \quad (1)$$

This means that the work done by the ventilator within each cycle to introduce air into the respiratory system coincides with the area under the curve of the inspiratory limb of the pressure-volume dynamic loop, measured on the volume axis. This work is exactly the energy that the ventilator supplies to the patient's respiratory system in order to ventilate it. Based on this understanding, Gattinoni et al.¹⁶ obtained two formulae capable of estimating MP during volume control ventilation; these formulae are very easy to calculate. The formulae adapt the classical respiratory physiology equation of movement with a geometric model of the pressure–volume loop (available currently in most mechanical ventilators) (Fig. 1).¹⁷ The

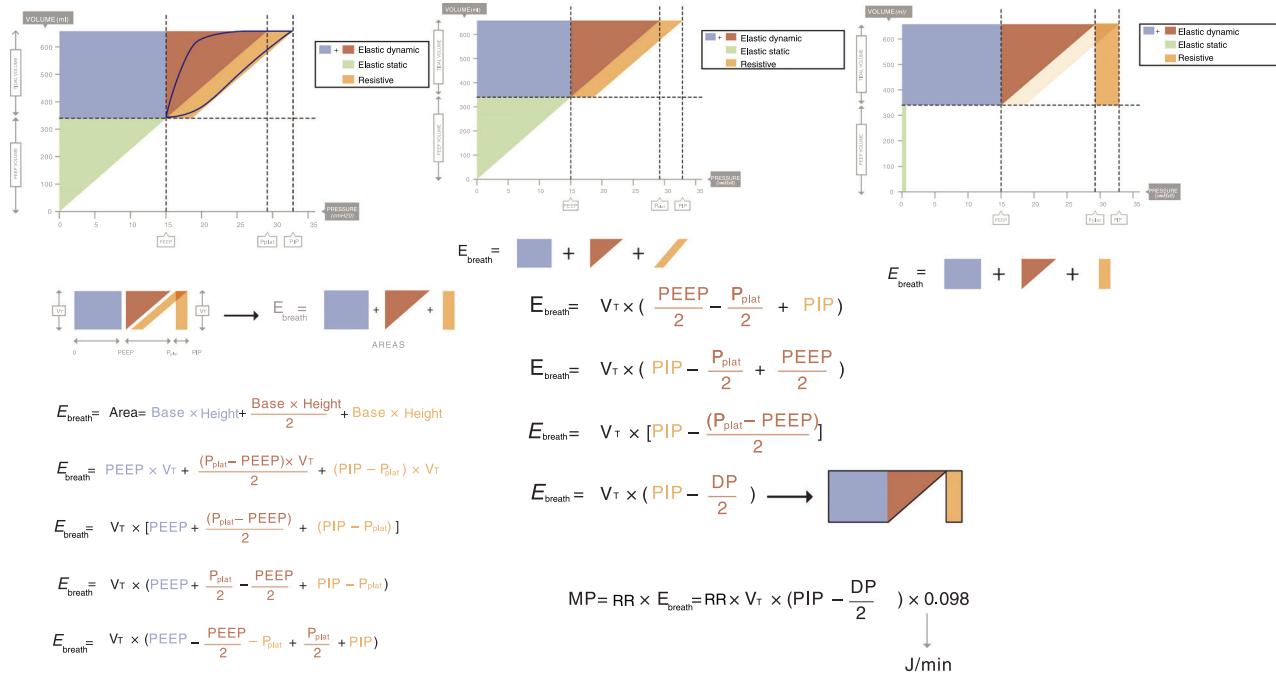


Figure 1 Mechanical power calculation. From a practical point of view, the elastic triangle (green triangle) is not included in the energy calculation because this energy is only used in the first inspiration. The key point is the energy which is delivered in the following consecutive breaths. PEEP: positive end-expiratory pressure; E_{breath} : energy supplied in each breath; V_T : tidal volume; P_{plat} : plateau pressure; PIP: peak inspiratory pressure; DP: driving pressure.

energy supplied (J) in each cycle using a constant-flow modality is:

$$E_{\text{breath}} (J) = V_T^2 \times (1/2 \times E + R/Ti) + V_T \times \text{PEEP} \quad (2)$$

E_{breath} : energy; V_T : tidal volume; E : elastance; R : resistance; Ti : inspiratory time; PEEP: positive end-expiratory pressure.

This equation is calculated in relation to two constants, elastance ($E = 1 \text{ C}^{-1}$) and resistance (R), but it can be simplified if we know that:

$$\text{Flow} = \frac{V_T}{Ti}.$$

$$\text{DP} = P_{\text{plat}} - \text{PEEP}.$$

$$R = \frac{\text{PIP} - P_{\text{plat}}}{\text{Flow}}.$$

$$E = \frac{\text{DP}}{V_T}.$$

Applying those concepts, it is possible to simplify the formula to:

$$E_{\text{breath}} (J) = V_T \times (\text{PIP} - 1/2 \times \text{DP}) \quad (3)$$

E_{breath} : energy; V_T : tidal volume; PIP: peak inspiratory pressure; DP: driving pressure.

Multiplying the energy supplied in each cycle by the RR mechanical power can be calculated:

$$\text{MP (J/min)} = E_{\text{breath}} (J) \times \text{RR (min}^{-1}\text{)}$$

MP: mechanical power; E_{breath} : energy; RR: respiratory rate.

As 0.098 is the conversion factor from L (from V_T) $\times \text{cmH}_2\text{O}$ (from the pressure) to Joules:

$$\text{MP (J/min)} = 0.098 \times \text{RR} \times [V_T^2 \times (1/2 \times E + R/Ti) + V_T \times \text{PEEP}] \quad (4)$$

MP: mechanical power; RR: respiratory rate; V_T : tidal volume; E : elastance; R : resistance; Ti : inspiratory time; PEEP: positive end-expiratory pressure.

Or its simplified equivalent:

$$\text{MP (J/min)} = 0.098 \times \text{RR} \times V_T \times (\text{PIP} - 1/2 \times \text{DP}) \quad (5)$$

MP: mechanical power; RR: respiratory rate; V_T : tidal volume; PIP: peak inspiratory pressure; DP: driving pressure.

In this article, Gattinoni demonstrated that the resulting calculation of these formulae is equivalent to the area under the curve of the dynamic pressure-volume loop, on the volume axis (work of breathing), both in normal lungs and in patients with ARDS. Using computer simulation models he also concluded that:

- MP increases exponentially:
 - With V_T , DP and Flow (exponent = 2).
 - With RR (exponent = 1.4).
- MP increases linearly: with PEEP, E and R .

In the same year, the same research team published¹⁸ a proof of concept study that concluded that MP is the cause of VILI. That study consisted of two experiments.

- The first experiment identified a MP threshold above which VILI is produced. They studied mechanically ventilated pigs, ventilated in volume control for 54 h with a strain ≥ 2 (previously thought to develop VILI and cause death at RR of 15 bpm) and divided them into 5 cohorts. Each of the cohorts was ventilated with a different RR (3, 6, 9, 12 and 15 bpm), producing different mechanical powers ($2 \pm 0.2 \text{ J}$, $7 \pm 3 \text{ J}$, $10 \pm 3 \text{ J}$, $14 \pm 2 \text{ J}$ and $22 \pm 2 \text{ J}$). The production of VILI was identified using CT scan and with histology. Only when MP was greater than 12 J/min was VILI produced. Below that threshold, there was no pathology. The experiment was shortened due to the death of the pigs ventilated at higher MP.
- The second experiment was a confirmation experiment to demonstrate that RR is not the single factor in the production of VILI. This time, all pigs were ventilated at 35 bpm for 54 h and divided into two cohorts based on the effects of V_T on MP. In the first group the MP was less than 12 J/min ($8 \pm 2 \text{ J/min}$) and in the other group, MP was greater than 12 J/min ($22 \pm 5 \text{ J/min}$). The results confirmed the findings of the first experiment: VILI was induced in the high MP cohort, where stress, strain, E_{breath} , and dynamic hysteresis rates increased during MV (i.e. the duration of ventilation worsened VILI).

In addition, data from both experiments demonstrated that the MP supplied is inversely proportional to the oxygenation drop (P/F) and directly proportional to the increase in elastance, viscous behaviour indexes (P1–P2 difference, dynamic hysteresis) and the anatomopathological measures of pulmonary injury.

The existence of this MP threshold is an extremely relevant finding and is compatible with what is already known in material science.^{19–21} In any material, there are always impurities (sometimes microscopic) that act as stress raisers and contribute to the formation of internal fractures. From these initial points of rupture, the extension of fractures follows the so-called Griffith fracture criterion where the energy has to increase over a certain threshold to propagate the fracture. This extension produces fatigue within the material. The analogy of this theory with MP and VILI is clear.

The scientific evidence of the role of MP in VILI development is still not very robust but it points strongly in that direction. In the LUNG SAFE²² cohort, the use of PEEP was independently associated with decreased mortality, and elevated RR, PIP and DP increased mortality. All

those parameters are included in the abbreviated formula of MP.

Another study by Fuller et al.²³ found that in patients with healthy lungs in which a protective ventilation strategy was applied, both increased DP and MP were associated with the development of ARDS.

The identification of a MP threshold from which VILI is generated seems to be very relevant for strategies at the bedside.

The use of high frequency oscillation ventilation (HFOV) seems to be a paradigmatic everyday example. Based on volu/barotrauma theories, the use of HFOV should be safer and less harming than conventional mechanical ventilation (CMV) as V_T is delivered below dead space with a moderate continuous distending pressure (MAP). Contrary to that theory, the current available literature has not demonstrated superiority and has even shown worse outcomes when using HFOV against CMV. This paradox can be explained by the energy transmission in HFOV. As the modality uses simple harmonic motion to deliver ventilation, the energy transmitted by this wave can exceed the MP threshold for VILI formation.

This assumption, based on the new theory, is only a hypothesis awaiting experimental confirmation. The same principles may, in the future, be used to refine the criteria for respiratory ECLS in patients with ARDS.

Thermodynamic theory: lung injury as a product of generated Entropy

Aside from all these studies, Oliveira et al.²⁴ published an alternative version of the same theory from the point of view of thermodynamics. Thermodynamics is the part of physics that deals with the mechanical action or relations to heat. For a better understanding, it is necessary to consider that a lung that is artificially ventilated does obey the laws of thermodynamics as it transitions from one state (expiration) to another (inspiration) and vice versa. To understand this reasoning, it is only necessary to understand the first two laws of thermodynamics:

- First law of thermodynamics. This is the law of conservation of energy. Energy cannot be created or destroyed, only changed in form. This applies to the internal energy of a thermodynamic system and how it changes. According to this law there are only two ways of changing the internal energy of a closed, i.e. one that is unable to exchange matter, thermodynamic system:

1. Heating it (or cooling it) with a certain amount of thermal energy (Q).
2. Doing work (W).

$$\Delta\text{Energy (J)} = \Delta Q (\text{J}) + \Delta W (\text{J}) \quad (6)$$

Q : thermal energy; W : work.

- Second law of thermodynamics. In a repeated process, there will always be some energy that cannot be

converted into work. This explains the generation of entropy (S), which is the amount of thermal energy that cannot be converted into work. When a change of state occurs, the entropy of a system can never decrease. If entropy has to be calculated in relation to absolute temperature (in Kelvin degrees), this formula must be used:

$$\Delta S (\text{J}) = \frac{\Delta Q}{T}; \quad \Delta Q (\text{J}) = \Delta S \times T \quad (7)$$

S : entropy; T : temperature; Q : thermal energy.

Combining both laws, the equation for the state of a thermodynamic system is obtained:

$$\Delta\text{Energy (J)} = \Delta S \times T + \Delta W \quad (8)$$

S : entropy; T : temperature; W : work.

This equation describes the relationship between internal energy, temperature, entropy and the work done by (or on) a thermodynamic system.

The essence of a living being is a continuous internal activity of an extremely organised nature (electrical, chemical and temperature gradients). In 1944, the book "What is life?" by Erwing Schrödinger stated that, from the thermodynamic point of view, living beings are able to maintain order throughout their lives in an apparent violation of the second law of thermodynamics. For that, they must be able to transfer to the environment around them the entropy they are generating. However, what happens if not all the entropy can be exported? The remaining entropy is retained within the system and its inevitable consequence is the gradual progression of the system towards dysfunction (i.e. illness) and eventual death. This raises two essential questions about the life and death of an organism: at what rate is entropy produced within an organism and how effective is that organism at exporting the entropy generated? This philosophical explanation has been considered at a lung level by Oliveira et al.

For thermodynamics,²⁵ an entropy generator is a system composed of two parts that are in contact. This is an example (electronic Fig. 2):

1. The first part is a weight of mass m that is submerged in a viscous liquid and is falling inside it. During the fall, it rotates a set of paddles.
2. The second part is a heat reservoir that maintains a constant temperature T and is in thermal contact with part 1. For thermodynamics, a "heat reservoir" is capable, by definition, of keeping the temperature constant regardless of how much it is heated or cooled. It has an infinite capacity to absorb heat.

When the mass of weight m falls (because of the effect of gravity, g) a distance h , a work W is done on the inside of the viscous liquid:

$$W = m \times h \times g \quad (9)$$

W : work; m : mass; h : distance; g : gravity.

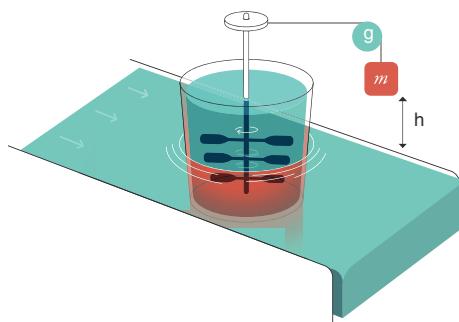


Figure 2 Entropy generator. Reproduced with permission Modesto-Alapont et al.¹⁷
m: mass; h: distance; g: gravity.

This produces an increase in the thermal energy of the viscous liquid which would lead to an increase in its temperature because of the existence of the heat reservoir. Since the liquid and the reservoir are in thermal contact and the reservoir maintains its constant temperature, when the weight drops, the liquid transfers that energy in the form of heat to the reservoir thus causing the entropy of the reservoir to increase.

$$\frac{W}{T} = \frac{m \times h \times g}{T} \quad (10)$$

W: work; T: temperature; m: mass; h: distance; g: gravity.

If the liquid is able to transfer that entropy to the reservoir, its entropy remains constant. The "entropy generator" demonstrates that when a work (W) is completely dissipated in a heat reservoir of temperature (T), the entropy of the complete system (liquid + reservoir) increases by a quantity (W/T).

The system formed by the lung and the circulatory system can be described as an entropy generator:

1. Respiratory system. The liquid moved by the paddles would represent the lung subjected to the respiratory work ($W_{OB} = E_{breath}$) produced by the mechanical ventilator in every inspiration. It is important to remember that the mechanical power (MP) is the energy multiplied by the respiratory rate.
2. Circulatory system. This system acts as the calorific reservoir that is in thermal contact with the lungs and is able to maintain constant body temperature (isothermal conditions at 36.5°C , $273.15 \pm 36.5^{\circ}\text{C} = 309.65^{\circ}\text{K}$).

As long as the lung is able to export the entropy to the circulatory system, dissipating completely the work done on itself, the pulmonary entropy remains constant: VILI will not be produced. However, if the MP is too high and exceeds the capacity of the circulatory system to remove the entropy that is occurring inside the lung, part of the entropy generated (MP/T) produces VILI in the lung. Therefore, the ability of the circulatory system to eliminate entropy generated

inside the lung explains why there is a threshold of MP from which VILI is generated.

Oliveira et al. postulated that if the lung moves within the elastic limit (with a small strain), the three-dimensional distribution of the microscopic fibres of elastin and collagen of the interior of the lung tissue causes the stress to fall almost exclusively on the elastin fibres. Elastin fibres have a very characteristic thermodynamic property: they behave like elastic rubber bands and have a Young's modulus proportional to their absolute temperature (T). This means that:

- When they are stretched during normal breathing (inspiration) they are able to release heat to the environment that surrounds them (circulatory system), decreasing their entropy.²⁶
- During contraction (expiration), they can recover the thermal energy from the circulatory system and transform it into work thus returning the system to equilibrium.

If the lung is ventilated, applying energy (MP) in the range where the lung behaves like an elastic solid, all the energy provided during inspiration is recovered at the end of expiration without losses. Entropy is not generated. The process is reversible and VILI does not occur.

On the other hand, if the amount of energy applied turns the lung into a viscous liquid, the mechanism of the "entropy generator" starts. In this case, stress also falls on the collagen fibres which are approximately 100 times more rigid than elastin and hyaluronic acid, one of the weakest structures of the extracellular matrix of the lung.

As long as the circulatory system is capable of removing the entropy (MP/T) generated inside the lung, VILI is not produced. However, if the MP is too high and the capacity of the circulatory system to withdraw is saturated, then the entropy irreversibly deforms the parenchyma and produces VILI.

Knowing that:

- The hyaluronic acid molecular weight is 2500 Da.
- The human lung possesses 0.1×10^{-6} g of hyaluronic acid for each gram of lung tissue.
- The force needed to break the bonds between hyaluronic acid and its surrounding proteins is $(40 \pm 11) \times 10^{-12}$ N.

Gattinoni et al.²⁷ calculated that to displace the hyaluronic protein's bond by 2.8×10^{-6} m, 1.12×10^{-16} J are needed.

When MP is 12 J/min, the entropy generated at 36.5°C is $12/309.65^{\circ}\text{K} = 0.038$ J/min. If the entropy is divided by number of molecules of hyaluronic acid affected, the energy applied to each molecule is approximately the same as the necessary energy to break their bond with the proteins. It is likely that each respiratory cycle is breaking a higher

number of molecules than those that can be repaired physiologically. If MP increases, and with it the entropy divided by molecules, the rhythm at which fractures are generated exceeds the physiological capacity for repair and VILI is produced.

Conclusion

A new theory to explain VILI has been developed in recent years based on the knowledge of the physical changes generated by rheology, material science and thermodynamics. It has been evaluated experimentally in animal models but also, when the concept is applied to existing studies in mechanically ventilated humans, it can explain the facts and phenomena described in those patients more completely than the more established theories (barotrauma, volutrauma, atelectrauma and biotrauma).

The main component is the existence of an energy (MP) threshold above which VILI will be generated. In the near future, this is likely to revolutionise the indications and application of different modes of MV and may inform the thresholds for consideration of extracorporeal respiratory support.

Conflicts of interest

The authors declare that they have no conflicts of interest.

References

1. Protti A, Andreis DT, Monti M, Santini A, Sparacino CC, Langer T, et al. Lung stress and strain during mechanical ventilation: any difference between statics and dynamics? *Crit Care Med.* 2013;41:1046–55.
2. Cressoni M, Chiurazzi Ch, Gotti M, Amini M, Brioni M, Algieri I, et al. Lung inhomogeneities and time-course of ventilator-induced mechanical injuries. *Anesthesiology.* 2015;123: 618–27.
3. Mead J, Takishima T, Leith D. Stress distribution in lungs: a model of pulmonary elasticity. *J Appl Physiol.* 1970;28: 596–608.
4. Hotchkiss JR, Blanch L, Murias G, Adams AB, Olson DA, Wan-genstein OD, et al. Effects of decreased respiratory frequency on ventilator-induced lung injury. *Am J Respir Crit Care Med.* 2000;161:463–8.
5. Retamal J, Borges JB, Bruhn A, Cao X, Feinstein R, Hedenstierna G, et al. High respiratory rate is associated with early reduction of lung edema clearance in an experimental model of ARDS. *Acta Anaesthesiol Scand.* 2016;60: 79–92.
6. Protti A, Maraffi T, Milesi M, Votta E, Santini A, Pugni P, et al. Role of strain rate in the pathogenesis of ventilator-induced lung edema. *Crit Care Med.* 2016;44: e838–45.
7. Maeda Y, Fujino Y, Uchiyama A, Matsuura N, Mashimo T, Nishimura M. Effects of peak inspiratory flow on development of ventilator-induced lung injury in rabbits. *Anesthesiology.* 2004;101:722–8.
8. Fujita Y, Maeda Y, Fujino Y, Uchiyama A, Mashimo T, Nishimura M. Effect of peak inspiratory flow on gas exchange, pulmonary mechanics and lung histology in rabbits with injured lungs. *J Anesth.* 2006;20:96–101.
9. Fujita Y, Fujino Y, Uchiyama A, Mashimo T, Nishimura M. High peak inspiratory flow can aggravate ventilator-induced lung injury. *Med Sci Monit.* 2007;13: BR95–100.
10. Protti A, Cressoni M, Santini A, Langer T, Mietto C, Febres D, et al. Lung stress and strain during mechanical ventilation. Any safe threshold? *Am J Respir Crit Care Med.* 2011;183: 1354–62.
11. Brunner JX, Wysocki M. Is there an optimal breath pattern to minimize stress and strain during mechanical ventilation? *Intensive Care Med.* 2009;35:1479–83.
12. Gattinoni L, Caironi P, Cressoni M, Chiumello D, Ranieri VM, Quintel M, et al. Lung recruitment in patients with acute respiratory distress syndrome. *N Engl J Med.* 2006;354: 1775–86.
13. Kassis EB, Loring SH, Talmor D. Mortality and pulmonary mechanics in relation to respiratory system and transpulmonary driving pressures. *Intensive Care Med.* 2016;42: 1206–13.
14. Retamal J, Borges JB, Bruhn A, Feinstein R, Hedenstierna G, Suarez-Sipmann F, et al. Open lung approach ventilation abolishes the negative effects of respiratory rate in experimental lung injury. *Acta Anaesthesiol Scand.* 2016;60: 1131–41.
15. Marini JJ, Rodriguez M, Lamb V. Bedside estimation of the inspiratory work of breathing during mechanical ventilation. *Chest.* 1986;89:56–63.
16. Gattinoni L, Tonetti T, Cressoni M, Cadringher P, Herrmann P, Moerer O, et al. Ventilator-related causes of lung injury: the mechanical power. *Intensive Care Med.* 2016;42: 1567–75.
17. Modesto-Alapont V, Medina A, Aguar-Carrascosa M, Vidal-Micó S, Vivanco-Allende A, Betes-Mendicute M. Respiratory physiology. The physics of mechanical ventilation. In: Medina A, Humphry A, Christpherson M, García Cuscó M, editors. *Handbook of paediatric and neonatal mechanical ventilation.* 1.^a edición electrónica Oviedo: Tesela ediciones; 2018 (Chapter 1).
18. Cressoni M, Gotti M, Chiurazzi C, Massari D, Algieri I, Amini M, et al. Mechanical power and development of ventilator-induced lung injury. *Anesthesiology.* 2016;124: 1100–8.
19. Sun CT, Jin ZH. Fracture mechanics. 1st ed. Massachusetts, USA: Academic Press/Elsevier; 2012.
20. Anderson TL. Fracture mechanics: fundamentals and applications. 3rd ed. Boca Raton, Philadelphia, USA: Taylor & Francis; 2005.
21. Freund LB. Dynamic fracture mechanics. Cambridge: Cambridge University Press; 1990.
22. Laffey JF, Bellani G, Pham T, Fan E, Madotto F, Bajwa EK, et al. Potentially modifiable factors contributing to outcome from acute respiratory distress syndrome: the LUNG SAFE study. *Intensive Care Med.* 2016;42: 1865–76.
23. Fuller BM, Page D, Stephens RJ, Roberts BW, Drewry AM, Abordeppey E, et al. Pulmonary mechanics and mortality in mechanically ventilated patients without acute respiratory distress syndrome: a cohort study. *Shock.* 2018;49: 311–6.

24. Oliveira CLN, Araújo AD, Bates JHT, Andrade JS Jr, Suki B. Entropy production and the pressure–volume curve of the lung. *Front Physiol.* 2016;7:73.
25. Lemon DS. A Student's guide to entropy. 1st ed. Cambridge: Cambridge Univ Press; 2013.
26. Callen HB. Thermodynamics and an introduction to thermo-statistics. 2nd ed. NY: John Wiley; 1985.
27. Tonetti T, Vasques F, Rapetti F, Maiolo G, Collino F, Romitti F, et al. Driving pressure and mechanical power: new targets for VILI prevention. *Ann Transl Med.* 2017;5:286.